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(54) Steel pipe having low yield ratio

(57) The present invention provides a steel pipe having a low yield ratio and is: a steel pipe having a low yield ratio, wherein the steel pipe contains, in mass, 0.01 to 0.20% C, 0.05 to 1.0% Si, 0.1 to 2.0% Mn and 0.001 to 0.05% Al, the microstructure of the steel pipe is composed of ferrite and pearlite, or ferrite and cementite, and the average size of the ferrite grains is not smaller than 20 μm; and a steel pipe having a low yield ratio, wherein the steel pipe contains, in mass, 0.03 to 0.20% C, 0.05 to 1.0% Si, 0.1 to 2.0% Mn, 0.001 to 0.05% Al, 0.01 to 0.5% Nb and 0.001 to 0.01% N, the microstructure of the steel pipe is composed of ferrite and bainite, or ferrite, martensite and bainite, or ferrite and martensite, and the average size of the ferrite grains is not smaller than 20 μm.

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Description

[0001] The present invention relates to a steel pipe having a low yield ratio.

[0002] It has been clarified recently that it is effective to use a steel material having a low yield ratio, as a structural member, to enhance the earthquake resistance of a building. In that sense, a steel pipe for a building is also requited to have a low yield ratio.
This is because it is estimated that if the yield ratio of a steel pipe for a building is lower, the steel pipe will seldom rupture, even though it yields, and therefore the structure is less likely to be destroyed.

[0003] In the case of a line pipe, highly reliable impact resistance and earthquake resistance are required of a line pipe to avoid the leakage of a transported material such as petroleum or the bursting of the line pipe. In that sense, it is effective to use a steel pipe having a low yield ratio as a line pipe for greater safety.

[0004] In the meantime, with regard to a welded steel pipe, as a welded steel pipe undergoes the influence of cold-working such as bending, pipe expansion, drawing and so on. during pipe production, a welded steel pipe having the same low yield ratio as a steel sheet used as the mother material of the steel pipe cannot be obtained, in many cases. Therefore, to obtain a steel pipe having a low yield ratio, it is necessary to sufficiently lower the yield ratio of a steel sheet before it is used in pipe production.

[0005] In JP-A-10-17980, a method is disclosed wherein, in the event of producing a welded steel pipe having a low yield ratio, a steel containing 1 to 3% Cr as an essential component is used as the base steel and the structure of the steel is composed of a composite structure containing a soft ferrite phase and a hard bainite or martensite phase in a manner that is already known.

[0006] In JP-A-2000-54061, it is described that a steel material and a steel pipe made of the steel material, that have a low yield ratio at the ordinary temperature and are excellent in strength at a high temperature, can be obtained by controlling the C contained in the steel material to not more than 0.03%, preferably not more than 0.015%, making Nb exist in the state of solid solution and, further, properly controlling the microstructure of the steel material.

[0007] In JP-A-2000-239972, it is described that a steel material and a steel pipe made of the steel material, that have a low yield ratio at the ordinary temperature and are excellent in strength at a high temperature, can be obtained by controlling the C contained in the steel material to not more than 0.02%, preferably not more than 0.015%, and adding Nb and Sn abundantly.

[0008] The above-mentioned method of JP-A-10-17980 requires Cr of not less than 1% as an essential component in order to secure a low yield ratio and a high strength simultaneously by forming a hard phase composed of a bainite phase or a martensite phase. However, the invention cannot provide a low cost steel pipe having a low yield ratio because Cr alloy is expensive. In addition, Cr tends to form oxides during welding and when Cr oxides remain at a weld-butting portion, the quality of a weld deteriorates.

[0009] In the methods according to JP-A-2000-54061 and JP-A-2000-239972, a low yield ratio is secured by limiting the upper limit of C to not more than 0.03% and 0.02% respectively, preferably not more than 0.015%, and, by so doing, reducing the amount of solute G at the ordinary temperature. However, in such cases of reducing the C amount as described above, a high tensile strength is seldom obtained in a tensile test at the ordinary temperature.

[0010] The object of the present invention is, by solving the above problems, to provide a steel pipe having a low yield ratio, and the gist thereof is as follows:

(1) A steel pipe having a low yield ratio, characterized in that: the steel pipe contains, in mass, 0.01 to 0.20% C, 0.05 to 1.0% Si, 0.1 to 2.0% Mn and 0.001 to 0.05% Al, with the balance consisting of Fe and unavoidable impurities; the microstructure of the steel pipe is composed of ferrite and additionally one or both of pearlite and cementite; and the average size of the ferrite grains is not smaller than 20 μm.

(2) A steel pipe having a low yield ratio according to the item (1), characterized in that the microstructure of the steel pipe contains spheroidized pearlite or spheroidized cementite.

(3) A steel pipe having a low yield ratio according to the item (2), characterized in that the average size of pearlite grains or cementite crystal grains is not larger than 20 μm.

(4) A steel pipe having a low yield ratio according to any one of the items (1) to (3), characterized in that the steel pipe contains, in mass, one or both of 0.01 to 0.5% Nb and 0.001 to 0.01% N.

(5) A steel pipe having a low yield ratio, characterized in that: the steel pipe contains, in mass, 0.03 to 0.20% C, 0.05 to 1.0% Si, 0.1 to 2.0% Mn, 0.001 to 0.05% Al, 0.01 to 0.5% Nb and 0.001 to 0.01% N, with the balance consisting of Fe and unavoidable impurities; the microstructure of the steel pipe is composed of ferrite and bainite; and the average size of the ferrite grains is not smaller than 20 μm.

(6) A steel pipe having a low yield ratio according to the item (5), characterized in that the content rate of bainite is, in volume fraction, in the range from 1 to 15%.

(7) A steel pipe having a low yield ratio, characterized in that: the steel pipe contains, in mass, 0.03 to 0.20% C, 0.05 to 1.0% Si, 0.1 to 2.0% Mn, 0.001 to 0.05% Al, 0.01 to 0.5% Nb and 0.001 to 0.01% N, with the balance

consisting of Fe and unavoidable impurities; the microstructure of the steel pipe is composed of ferrite, martensite and bainite, or ferrite and martensite; and the average size of the ferrite grains is not smaller than 20 μm.

(8) A steel pipe having a low yield ratio according to the item (7), characterized in that the content rate of bainite is, in volume fraction, in the range from 1 to 15% and/or that of martensite is, in volume fraction, in the range from 1 to 15%.

(9) A steel pipe having a low yield ratio according to any one of the items (1) to (8), characterized in that the steel pipe contains, in mass, one or both of 0.005 to 0.1% Ti and 0.0001 to 0.005% B.

(10) A steel pipe having a low yield ratio according to any one of the items (1) to (9), characterized in that the steel pipe contains, in mass, one or more of 0.01 to 0.5% V, 0.01 to 1% Cu, 0.01 to 1% Ni, 0.01 to 1% Cr and 0.01 to 1% Mo.

THE MOST PREFERRED EMBODIMENT

[0011] The feature common to the whole present invention is that the microstructure of a steel pipe is composed of a structure containing ferrite and the average size of the ferrite grains is not smaller than 20 μm. As a yield stress is proportioned to (grain size)$^{-1/2}$ according to Hall-Petch's Law, a yield stress and a yield ratio increase as a grain size decreases. In contrast with this, a yield stress and a yield ratio decrease as a grain size increases. The present invention, based on the above fact, has made it clear that, when the average size of ferrite grains contained in a microstructure is not smaller than 20 μm, a yield stress lowers and as a result a low yield ratio can be obtained even with a steel pipe after subjected to pipe production processes. An average size of ferrite grains is preferably not smaller than 30 μm, still preferably not smaller than 40 μm.

[0012] The average size of grains including ferrite grains is measured in accordance with the method described in the Appendix 1 of JIS G 0552. In the case of martensite or bainite, the size of prior austenite grains is measured and it is recommended to conform to the Appendix 3 of JIS G 0551.

[0013] It is preferable that the content rate of ferrite in a microstructure is in the range from 70 to 98%. The reason is that, when the content rate of ferrite is less than 70%, a yield stress cannot be lowered sufficiently even with a ferrite grain size increased and therefore a low yield ratio cannot be obtained. However, when the content rate of ferrite exceeds 98%, the tensile strength of a steel lowers and therefore a low yield ratio cannot be obtained likewise. It is still preferable that the content rate of ferrite is in the range from 75 to 95%.

[0014] Here, the content rate of ferrite, bainite or martensite in a microstructure in the present invention means a volume traction of ferrite, bainite or martensite in the microstructure, respectively.

[0015] In conventional hot rolling of a steel sheet used for producing a steel pipe having a low yield ratio, the steel sheet has been rolled in the temperature range from a temperature of the γ phase region to a lower side temperature of the two-phase region after it is heated to a temperature of the γ phase region. Therefore, it has been impossible to make the average ferrite grain size not smaller than 20 μm. The present invention has made it possible to: finish rolling in the temperature range from a temperature of the γ phase region to a higher side temperature of the two-phase region after a steel is heated to a temperature of the γ phase region; thus suppressing the fractionization of grains; and, as a result, produce a steel having an average ferrite grain size of not smaller than 20 μm. It is possible to make the average ferrite grain size not smaller than 20 μm by controlling a cooling rate to not more than 10°C/sec. up to the temperature of the Ar_1 point + 50°C after the end of hot rolling.

[0016] Furthermore, it is possible to make the average ferrite grain size not smaller than 30 or even 40 μm by controlling a temperature at the end of hot rolling, a cooling rate after the end of hot rolling, and so on.

[0017] The present invention is constituted of: the first invention wherein a microstructure is composed of ferrite and additionally one or both of pearlite and cementite; the second invention wherein a microstructure is composed of ferrite and bainite; and the third invention wherein a microstructure is composed of ferrite, martensite and bainite, or ferrite and martensite. Each invention is hereunder explained in detail.

[0018] The first invention is explained hereunder.

[0019] In the first invention, a microstructure is composed of ferrite and additionally one or both of pearlite and cementite. That means that the microstructure is a structure that contains ferrite as an essential phase and additionally one or both of pearlite and cementite. As a result of composing such a structure, a steel pipe having a low yield ratio and a tensile strength of 500 to 600 MPa can be produced.

[0020] The reasons for limiting the chemical components in the first invention are explained hereunder.

[0021] C is an element that precipitates as solid solution or carbides in a matrix and enhances the strength of a steel. Further, C precipitates also as the second phase composed of cementite and pearlite. Therefore, in the event of forming a hot-rolled steel sheet into a steel pipe by cold forming, C suppresses the increase of a yield stress or proof stress, enhances tensile strength and uniform elongation, and resultantly contributes to the lowering of a yield ratio. C is required to be contained at not less than 0.01%, preferably not less than 0.04%, for securing the effect of cementite, etc. precipitating as the second phase on the lowering of a yield ratio. However, when C is contained in excess of

0.20%, the effect of lowering a yield ratio and weldability deteriorate. For these reasons, a C content is limited to the range from 0.01 to 0.20%.

[0022] Si functions as a deoxidizer and enhances the strength of a steel by dissolving in a matrix. The effect appears with a Si content of not less than 0.05%. On the other hand, when Si exceeds 1.0%, the effect of lowering a yield ratio deteriorates. For these reasons, the Si content is limited to the range from 0.05 to 1.0%.

[0023] Mn is an element that enhances the strength of a steel and accelerates the precipitation of cementite or pearlite composing the second phase. The effects appear with a Mn content of not less than 0.1%. On the other hand, when Mn is contained in excess of 2.0%, the effect of lowering a yield ratio deteriorates. For these reasons, the Mn content is limited to the range from 0.1 to 2.0%. Here, from the viewpoint of strength and toughness, it is preferable that the Mn content is in the range from 0.3 to 1.5%.

[0024] Al is used as a deoxidizer but the amount of Al significantly influences a grain size and mechanical properties. An Al content of less than 0.001% is insufficient as a deoxidizer. On the other hand, when Al exceeds 0.05%, oxides containing A1 increase in a steel and deteriorate toughness. For these reasons, the Al content is limited to the range from 0.001 to 0.05%.

[0025] A microstructure composed of ferrite and additionally one or both of pearlite and cementite according to the first invention is obtained by: finishing rolling in the temperature range from a temperature of the γ phase region to a higher side temperature of the γ-α two-phase region after a steel is heated to a temperature of the γ phase region; thereafter cooling the steel at a cooling rate of not more than 10°C/sec. up to the temperature of the Ar_1 point + 50°C; and successively cooling the steel at a cooling rate of not less than 3°C/sec. in the temperature range not higher than the temperature of the Ar_1 point + 50 °C.

[0026] In the first invention, it is preferable that a microstructure further contains spheroidized pearlite or spheroidized cementite. The reason is that, when such a structure is contained, the increase of a yield ratio can be suppressed in the event of forming a steel sheet into a steel pipe. In addition, spheroidized pearlite or spheroidized cementite has the effect of improving uniform elongation.

[0027] It can be determined whether pearlite or cementite is spheroidized or not by defining pearlite or cementite as it is spheroidized when an aspect ratio between the length and the width of the second phase is not more than 2 in a section parallel with the rolling direction.

[0028] The spheroidization of pearlite or cementite can be done by: heating a steel material to a temperature in the range of 1,150°C ± 50°C; thereafter finishing the hot rolling of the steel material at a temperature of not lower than the Ar_1 point and thus producing a steel strip about 10 mm in thickness to which strain (dislocation) is introduced; and successively cooling the steel strip at a cooling rate of 3 to 30°C/sec. up to a temperature of not higher than 700°C, then coiling it, and, in the meantime, precipitating cementite or pearlite at grain boundaries or on dislocations.

[0029] Further, in the first invention, it is preferable that the average size of pearlite grains or cementite grains is not larger than 20 μm. The reason is that, by so doing, the increase of a yield ratio can be suppressed in the event of forming a steel sheet into a steel pipe.

[0030] An average pearlite grain size of not larger than 20 μm can be obtained by controlling the cooling rate to not less than 3°C/sec. in the temperature range not higher than the temperature of the Ar_1 point + 50°C after the end of hot rolling.

[0031] Still further, in the first invention, it is preferable that a steel pipe contains one or both of 0.01 to 0.5% Nb and 0.001 to 0.01% N. Nb is an element that precipitates as solid solution or carbonitrides in a matrix and enhances strength, and therefore Nb is required to be contained by at least 0.01%. However, even though Nb is excessively added in excess of 0.5%, the effect is saturated and a sufficient strengthening effect is not secured or, instead, precipitates coarsen and toughness deteriorates. For these reasons, a Nb content is limited to the range from 0.01 to 0.5%. N exists as solid solution or nitrides in a matrix. A N content of not less than 0.001% is required for forming nitrides that contribute to the strengthening of a steel. However, when N is added in excess of 0.01%, coarse nitrides tend to form and deteriorate toughness. For these reasons, the N content is limited to the range from 0.001 to 0.01%.

[0032] Next, the second invention is explained hereunder.

[0033] In the second invention, a microstructure is composed of ferrite and bainite. As a result of composing such a structure, a steel pipe having a low yield ratio and a tensile strength of 600 to 700 MPa can be produced.

[0034] The reasons for limiting the chemical components in the second invention are explained hereunder.

[0035] C is an element that precipitates as solid solution or carbides in a matrix and enhances the strength of a steel. C is required to be contained by not less than 0.03% because the strength in a steel material of a heavy thickness is insufficient with the content of less than 0.03%, preferably C is requited to be contained by not less than 0.05%. However, when C is contained in excess of 0.20%, weldability deteriorates. For these reasons, a C content is limited to the range from 0.03 to 0.20%.

[0036] Si functions as a deoxidizer and enhances the strength of a steel by dissolving in a matrix. The effect appears with a Si content of not less than 0.05%. On the other hand, when Si exceeds 1.0%, the toughness of a steel material deteriorates. For these reasons, the Si content is limited to the range from 0.05 to 1.0%.

[0037] Mn is an element that enhances the strength of a steel and the effect appears with a Mn content of not less than 0.1%. A preferable content of Mn is not less than 0.3%. However, when Mn is contained in excess of 2.0%, toughness deteriorates caused by center segregation. For these reasons, the Mn content is limited to the range from 0.1 to 2.0%. Here, from the viewpoint of strength and toughness, it is preferable that the Mn content is in the range from 0.3 to 1.5%.

[0038] Al is used as a deoxidizer but the amount of Al significantly influences a grain size and mechanical properties. An Al content of less than 0.001% is insufficient as a deoxidizer. On the other hand, when Al exceeds 0.05%, oxides containing Al increase in a steel and deteriorate toughness. For these reasons, the Al content is limited to the range from 0.001 to 0.05%.

[0039] Nb is an element that precipitates as solid solution or carbonitrides in a matrix and enhances strength, and therefore Nb is required to be contained by at least 0.01%. However, even though Nb is excessively added in excess of 0.5%, the effect is saturated and a sufficient strengthening effect is not secured, or instead, precipitates coarsen and toughness deteriorates. For these reasons, a Nb content is limited to the range from 0.01 to 0.5%.

[0040] N exists as solid solution or nitrides in a matrix. A N content of not less than 0.001% is required for forming nitrides that contribute to the strengthening of a steel. However, when N is added in excess of 0.01%, coarse nitrides tend to form and deteriorate toughness. For these reasons, the N content is limited to the range from 0.001 to 0.01%.

[0041] A microstructure containing bainite according to the second invention is obtained by: heating a steel material to a temperature in the range of 1,150°C ± 100°C; thereafter hot rolling the steel material into a steel strip about 10 mm in thickness; thereafter cooling the steel strip at a cooling rate of not more than 10°C/sec. up to the temperature of the Ar_1 point + 50°C and thus causing ferrite transformation; successively cooling the steel strip at a cooling rate of not less than 5°C/sec. in the temperature range not higher than the temperature of the Ar_1 point + 50°C and thus forming bainite; and coiling the steel strip in the temperature range of not higher than 600°C.

[0042] In the second invention, it is preferable that the content rate of bainite is in the range from 1 to 15%. The reason is that, in a composite structure of ferrite and bainite, though the effect of lowering the increment of a yield ratio (YR) appears during the forming of a steel pipe when a bainite content rate is in the range from 1 to 15%, the effect does not appear with a bainite content rate of less than 1% and the YR increases with a bainite content rate of more than 15%. For these reasons, the content rate of bainite is limited to the range from 1 to 15%.

[0043] A bainite content rate in the range from 1 to 15% can be obtained by controlling the cooling rates up to the temperature of the Ar_1 point + 50°C and in the temperature range not higher than the temperature of the Ar_1 point + 50°C to the aforementioned conditions. If the cooling rates deviate from the aforementioned conditions, a bainite content rate rises or pearlite comes to be contained abundantly.

[0044] Note that a very small amount of pearlite or cementite may be contained in a composite structure of ferrite and bainite as far as the amount is in the range where the effect of lowering the increment of a yield ratio during the forming of a steel pipe is not hindered.

[0045] Further, in the second invention, it is preferable that the average size of bainite grains is in the range from 1 to 20 μm. The reason is that, by so doing, the increment of a yield ratio during the forming of a steel pipe can be lowered.

[0046] Next, the third invention is explained hereunder.

[0047] In the third invention, a microstructure is composed of ferrite, martensite and bainite, or ferrite and martensite. As a result of composing such a structure, a steel pipe having a low yield ratio and a tensile strength of 700 to 800 MPa can be produced.

[0048] The reasons for limiting the chemical components in the third invention are explained hereunder.

[0049] C is an element necessary for: precipitating as solid solution or carbides in a matrix and thus securing strength; and forming a hard phase of bainite and martensite and thus securing a low yield ratio. When a C content is less than 0.03%, a hard phase of bainite and martensite is not formed and thus a low yield ratio is not secured. Therefore, the C content not less than 0.03% is necessary. A preferable content thereof is not less than 0.05%. However, when C is contained in excess of 0.20%, weldability and toughness deteriorate. For these reasons, the C content is limited to the range from 0.03 to 0.20%.

[0050] Si functions as a deoxidizer and enhances the strength of a steel by dissolving in a matrix. The effect appears with a Si content of not less than 0.05%. On the other hand, when Si exceeds 1.0%, the toughness of a steel material deteriorates. For these reasons, the Si content is limited to the range from 0.05 to 1.0%.

[0051] Mn is an element that enhances the strength of a steel and the effect appears with a Mn content of not less than 0.1%. A preferable content of Mn is not less than 0.3%. However, when Mn is contained in excess of 2.0%, toughness deteriorates caused by center segregation. For these reasons, the Mn content is limited to the range from 0.1 to 2.0%. Here, from the viewpoint of strength and toughness, it is preferable that the Mn content is in the range from 0.3 to 1.5%.

[0052] Al is used as a deoxidizer but the amount of Al significantly influences a grain size and mechanical properties. An Al content of less than 0.001% is insufficient as a deoxidizer. On the other hand, when Al exceeds 0.05%, oxides containing Al increase in a steel and deteriorate toughness. For these reasons, the Al content is limited to the range

from 0.001 to 0.05%.

[0053] Nb is an element that precipitates as solid solution or carbonitrides in a matrix and enhances strength, and therefore Nb is required to be contained by at least 0.01%. However, even though Nb is excessively added in excess of 0.5%, the effect is saturated and a sufficient strengthening effect is not secured or, instead, precipitates coarsen and toughness deteriorates. For these reasons, a Nb content is limited to the range from 0.01 to 0.5%.

[0054] N exists as solid solution or nitrides in a matrix. A N content of not less than 0.001% is required for forming nitrides that contribute to the strengthening of a steel. However, when N is. added in excess of 0.01%, coarse nitrides tend to form and deteriorate toughness. For these reasons, the N content is limited to the range from 0.001 to 0.01%.

[0055] A microstructure composed of ferrite, martensite and bainite, or ferrite and martensite according to the third invention is obtained by: heating a steel material to a temperature in the range of 1,150°C ± 100°C; thereafter hot rolling the steel material into a steel strip about 10 mm in thickness and finishing the hot rolling at a temperature of not lower than the Ar_3 point; thereafter cooling the steel strip at a cooling rate of not more than 10°C/sec. up to the temperature of the Ar_1 point + 50°C and thus causing ferrite transformation; successively cooling the steel strip at a cooling rate of not less than 10°C/sec. up to a temperature of not higher than 600°C, preferably 500°C, still preferably 450°C, in the temperature range not higher than the temperature of the Ar_1 point + 50°C and thus forming bainite and/or martensite; and coiling the steel strip.

[0056] In the third invention, it is preferable that the content rate of bainite is in the range from 1 to 15% and/or the content rate of martensite is in the range from 1 to 15%. The reason is that, in a composite structure of ferrite and bainite and/or martensite, though the effect of lowering the increment of a yield ratio appears during the forming of a steel pipe when the content rate of bainite is in the range from 1 to 15% and/or the content rate of martensite is in the range from 1 to 15%, the effect does not appear with a bainite or martensite content rate of less than 1% and the YR increases with a bainite or martensite content rate of more than 15%. For these reasons, the content rate of bainite and/or that of martensite are limited to the range from 1 to 15%, respectively.

[0057] A bainite and/or martensite content rate in the range from 1 to 15% can be obtained by controlling the cooling rates up to the temperature of the Ar_1 point + 50°C and in the temperature range not higher than the temperature of the Ar_1 point + 50°C to the aforementioned conditions. If the cooling rates deviate from the aforementioned conditions, a bainite or martensite content rate rises or pearlite comes to be contained abundantly.

[0058] Now the reasons for limiting the preferable chemical components common to the first through third inventions are explained hereunder.

[0059] Ti is an element that has the effect of improving weldability and the effect is recognized with a Ti content of not less than 0.005%. However, when Ti is added in excess of 0.1%, the deterioration of workability and an unnecessary increase of strength are caused by the increase of Ti carbonitrides. For these reasons, the Ti content is limited to the range from 0.005 to 0.1%.

[0060] B causes grain boundary strengthening and precipitation strengthening by precipitating in the forms of $M_{23}(C, B)_6$, etc. and thus increases strength. The effect is low with a B content of less than 0.0001%. On the other hand, when the B content exceeds 0.005%, the effect is saturated, a coarse B-contained phase tends to form, and enbrittlement is likely to occur. For these reasons, the B content is limited to the range from 0.0001 to 0.005%.

[0061] V increases strength as a precipitationstrengthening element. The effect is insufficient with a V content of less than 0.01%. On the other hand, when a V content exceeds 0.5%, not only carbonitrides coarsen but also the increment of yield strength increases. For these reasons, the V content is limited to the range from 0.01 to 0.5%.

[0062] Cu is an element that increases strength. When a Cu content is less than 0.01%, the effect is low. On the other hand, when Cu is added in excess of 1%, the increment of yield strength increases. For these reasons, the Cu content is limited to the range from 0.01 to 1%.

[0063] Ni is an element that increases strength and also is effective for improving toughness. When a Ni content is less than 0.01%, the effect of improving toughness is low. On the other hand, when Ni is added in excess of 1%, the increment of yield strength increases. For these reasons, the Ni content is limited to the range from 0.01 to 1%.

[0064] Cr increases strength as a precipitationstrengthening element. The effect is insufficient with a Cr content of less than 0.01%. On the other hand, when the Cr content exceeds 1%, not only carbonitrides coarsen but also the increment of yield strength increases. For these reasons, the Cr content is limited to the range from 0.01 to 1%.

[0065] Mo causes solid solution strengthening and at the same time increases strength. When a Mo content is less than 0.01%, the effect is low. On the other hand, when Mo is added in excess of 1%, the increment of yield strength increases. For these reasons, the Mo content is limited to the range from 0.01 to 1%.

[0066] A steel according to the present invention can be provided in the forms of not only a steel pipe produced by cold-forming a hot-rolled steel sheet but also a steel plate and a steel sheet. Further, as an example of a product produced by cold-working a steel according to the present invention, an electric resistance welded steel pipe is nominated. With regard to the effects of the present invention, the effect of lowering a yield ratio is prominent when a low strain pipe forming method is employed.

EXAMPLE

Example 1

[0067] Example 1 relates to the first invention.

[0068] Steels having the components shown in Table 1 were produced into continuously cast slabs and then the slabs were hot rolled into steel sheets 10 mm in thickness. In the hot-rolling process: the slabs were heated to a temperature of 1,150°C; thereafter the hot rolling was finished at a temperature of 900°C (Ar_1 point + 170°C) and thus strain (dislocation) was introduced; successively the steel sheets were cooled at the cooling rates in the range from 5 to 15°C/sec. up to a temperature of not higher than 700°C; and then the steel sheets were coiled.

[0069] The microstructures of the steel sheets are shown in Table 2. The tensile properties of a steel sheet were evaluated by using an as-rolled specimen of the steel sheet to which no working was applied and a specimen thereof to which 5%-prestrain was applied. 5%-prestrain corresponds to the cold-working applied for forming a steel sheet 10 mm in thickness into a steel pipe 200 mm in diameter. In general, prestrain is applied so as to equal the value of t (steel pipe thickness)/D (steel pipe diameter) with respect to a steel pipe to be produced.
The prestrain was given by the method wherein a tensile test specimen was pulled with a tensile tester and the pulling was stopped at the time when the strain reached 5%. The tensile properties evaluated were YS (yield strength), TS (tensile strength) and YR (yield ratio). The results of the evaluation are shown in Table 2.

[Table 1]

	Symbol	Chemical components (mass%)											
		C	Si	Mn	Al	Cu	Ni	Cr	Mo	V	Nb	Ti	B
Invention example	A-1	0.15	0.25	1.30	0.023	0.005	0.006	0.004	0.006	0.005	0.004	0.002	0.00005
	B-1	0.14	0.35	1.25	0.030	0.004	0.005	0.005	0.004	0.007	0.005	0.003	0.00006
	C-1	0.12	0.31	1.12	0.025	0.006	0.007	0.006	0.005	0.006	0.006	0.001	0.00007
	D-1	0.12	0.28	1.08	0.020	0.005	0.005	0.004	0.004	0.005	0.006	0.003	0.00005
	E-1	0.08	0.41	0.85	0.019	0.007	0.006	0.005	0.005	0.004	0.004	0.012	0.00150
	F-1	0.13	0.32	0.72	0.025	0.005	0.020	0.410	0.560	0.303	0.071	0.001	0.00005
	G-1	0.07	0.34	0.80	0.036	0.540	0.650	0.005	0.005	0.215	0.056	0.020	0.00210
Comparative example	H-1	0.005	0.11	0.55	0.018	0.005	0.004	0.003	0.005	0.004	1.575	0.001	0.00005
	I-1	0.32	0.05	0.62	0.022	0.004	1.640	0.004	0.004	0.005	0.003	0.002	0.00004
	J-1	0.05	0.005	0.48	0.034	0.006	0.004	0.005	0.005	0.984	0.005	0.003	0.00005
	K-1	0.17	1.65	0.22	0.027	0.003	0.006	2.130	0.006	0.005	0.004	0.002	0.00006
	L-1	0.11	0.32	0.06	0.035	0.004	0.005	0.006	2.572	0.004	0.006	0.001	0.00004
	M-1	0.10	0.21	3.14	0.041	1.520	0.003	0.007	0.004	0.006	0.004	0.003	0.00003
	N-1	0.12	0.45	1.57	0.005	0.005	0.007	0.005	0.006	0.005	0.006	0.002	0.01025
	O-1	0.14	0.15	1.25	0.120	0.004	0.005	0.005	0.004	0.004	0.005	0.534	0.00004

[Table 2]

	Symbol	Microstructure			Tensile properties					
		Average ferrite grain size	Cementite or pearlite		As-rolled specimen			5%-prestrain specimen		
			Spheroidized or not	Average grain size	YS	TS	YR	YS	TS	YR
		(μm)		(μm)	(MPa)	(MPa)	(%)	(MPa)	(MPa)	(%)
Invention example	A-1	50	0	23	304	511	60	541	610	89
	B-1	41	1	10	281	506	55	423	558	76
	C-1	48	0	18	278	479	58	492	570	86
	D-1	54	1	9	254	475	53	388	523	74
	E-1	68	0	19	250	438	57	467	530	88
	F-1	45	0	18	283	518	55	497	609	82
	G-1	25	1	4	240	436	55	334	470	71
Comparative example	H-1	33	0	25	130	325	40	398	425	94
	I-1	30	0	31	344	564	61	648	673	96
	J-1	17	0	38	130	350	37	425	468	91
	K-1	24	0	35	418	571	73	668	685	97
	L-1	18	0	11	261	409	64	465	484	96
	M-1	17	0	32	321	479	67	567	589	96
	N-1	84	0	44	254	470	54	586	595	98
	O-1	10	0	5	336	452	74	477	509	94

Spheroidized or not
0: Not spheroidized
1: Spheroidized

[0070] In the cases of the invention examples Symbols A-1 to G-1, the steel components were within the ranges specified in the present invention and any of the average ferrite grain sizes was not smaller than 20 μm. The yield ratios (YRs) of the 5%-prestrain specimens were in the range from 71 to 89%. In the cases of Symbols B-1, D-1 and G-1 wherein pearlite or cementite was spheroidized, the YRs of the 5%-prestrain specimens were lower than the other specimens.

[0071] In the cases of the comparative examples Symbols H-1 to O-1, any of the steel components deviated from the ranges specified in the present invention. The average ferrite grain sizes were smaller than 20 μm in the cases of Symbols J-1, L-1, M-1 and O-1. These were the examples wherein YRs increased because YSs increased after 5%-prestrain was imposed. There were no cases where cementite or pearlite was spheroidized and, in the cases of Symbols H-1 to K-1, M-1 and N-1, the average grain sizes of the cementite or pearlite were outside the preferable range of not larger than 20 μm. These were the examples wherein pearlite or cementite that composed the second phase grew larger because the cooling rates were less than 3°C/sec. in the temperature range of not higher than Ar_1 point + 50°C after the end of hot rolling. Here, the yield ratios (YRs) of the 5%prestrain specimens were in the range from 91 to 98%. These were the examples wherein YSs increased and thus YRs increased because the grain sizes of cementite or pearlite that composed the second phase were large and therefore the cementite or pearlite grains acted as resistance to deformation when 5%-prestrain was imposed.

Example 2

[0072] Example 2 relates to the second invention.

[0073] Steels having the components shown in Table 3 were produced into continuously cast slabs and then the slabs were hot rolled into steel sheets 10 mm in thickness. In the hot-rolling process: the slabs were heated to a temperature of 1,150°C; thereafter the hot rolling was finished at a temperature of 900°C (Ar_1 point + 170°C); the steel sheets were cooled at the cooling rate of 5°C/sec. up to a temperature of 780°C (Ar_1 point + 50°C) and thus ferrite transformation was caused; successively the steel sheets were cooled at the cooling rate of 20°C/sec. in the temperature range of not higher than 780°C (Ar_1 point + 50°C) and thus bainite was formed; and then the steel sheets were coiled in the temperature range from 500°C to 600°C.

[0074] The microstructures of the steel sheets are shown in Table 4. The tensile properties of a steel sheet were evaluated by using an as-rolled specimen of the steel sheet to which no working was applied and a specimen thereof to which 5%-prestrain was applied. 5%-prestrain corresponds to the cold-working applied for forming a steel sheet 10 mm in thickness into a steel pipe 200 mm in diameter.

[0075] In general, prestrain is applied so as to equal the valve of t (steel pipe thickness)/D (steel pipe diameter) with respect to a steel pipe to be produced. The method of imposing prestrain and the conditions of the tensile tests were the same as Example 1. The results of the evaluation are shown in Table 4.

[Table 3]

	Symbol	Chemical components (mass%)												
		C	Si	Mn	Al	Nb	N	Cu	Ni	Cr	Mo	V	Ti	B
Invention example	A-2	0.07	0.22	1.12	0.018	0.021	0.0024	0.003	0.004	0.004	0.006	0.005	0.002	0.00005
	B-2	0.13	0.31	1.05	0.024	0.052	0.0030	0.005	0.001	0.005	0.004	0.007	0.003	0.00006
	D-2	0.11	0.24	0.94	0.021	0.031	0.0020	0.001	0.006	0.004	0.004	0.005	0.012	0.00153
	E-2	0.15	0.42	0.83	0.015	0.027	0.0030	0.123	0.534	0.004	0.006	0.004	0.012	0.00004
	F-2	0.11	0.38	0.75	0.027	0.034	0.0030	0.003	0.001	0.564	0.671	0.214	0.015	0.00027
Comparative example	H-2	0.005	0.12	0.45	0.023	1.575	0.0030	0.003	0.001	0.002	0.004	0.003	0.002	0.00004
	I-2	0.39	0.08	0.52	0.031	0.002	0.0020	0.005	1.684	0.003	0.005	0.004	0.003	0.00030
	J-2	0.04	0.005	1.24	0.018	0.005	0.0158	0.002	0.003	0.007	0.003	0.875	0.002	0.00005
	K-2	0.14	1.58	0.53	0.024	0.004	0.0020	0.006	0.004	2.260	0.006	0.003	0.001	0.00003
	L-2	0.10	0.28	0.05	0.017	0.006	0.0050	0.001	0.005	0.004	2.395	0.004	0.003	0.00002
	M-2	0.12	0.32	2.78	0.042	0.004	0.0030	1.640	0.007	0.005	0.003	0.005	0.002	0.00005
	N-2	0.11	0.52	1.48	0.004	0.006	0.0040	0.003	0.006	0.003	0.005	0.004	0.001	0.01058
	O-2	0.05	0.23	0.85	0.115	0.005	0.0050	0.004	0.002	0.002	0.002	0.003	0.456	0.00004

[Table 4]

	Symbol	Metallographic structure			Tensile properties					
		Structure composition	Average ferrite grain size	Bainite content rate	As-rolled specimen			5%-prestrain specimen		
					YS	TS	YR	YS	TS	YR
			(μm)	(volume%)	(MPa)	(MPa)	(%)	(MPa)	(MPa)	(%)
Invention example	A-2	α + B	46	0	311	440	71	369	468	79
	B-2	α + B	35	13	413	585	71	476	634	75
	D-2	α + B	38	12	381	540	70	442	589	75
	E-2	α + B	82	4	399	553	72	462	602	77
	F-2	α + B	41	10	406	608	67	469	657	71
Comparative example	H-2	α + P	13	0	245	310	79	304	326	93
	I-2	α + B	31	51	811	1119	72	1177	1293	91
	J-2	α + P	58	0	279	354	79	346	372	93
	K-2	α + B	33	38	704	959	73	919	987	93
	L-2	α + P	10	0	395	562	70	530	592	90
	M-2	α + B	32	29	708	877	81	868	903	96
	N-2	α + B	94	42	564	809	70	762	833	92
	O-2	α + P	8	0	303	375	81	369	392	94

α: Ferrite

B: Bainite

P: Pearlite

[0076] In the cases of the invention examples. Symbols A-2 to F-2, the steel components were within the ranges specified in the present invention, any of the structures was composed of ferrite and bainite, any of the average ferrite grain sizes was not smaller than 20 μm, and the content rates of bainite were in the preferable range of not more than 15%. The yield ratios (YRs) of the 5%prestrain specimens were in the range from 71 to 79%. In the cases where the content rates of bainite were high, though both YSs and TSs increased after 5%-prestrain was imposed, the increment of YSs was small in comparison with that of TSs and therefore YRs in those cases were lower than YRs in the cases where the content rates of bainite were low.

[0077] In the cases of the comparative examples Symbols H-2 to O-2, any of the steel components deviated from the ranges specified in the present invention. In the cases of Symbols H-2, J-2, L-2 and 0-2, the crystal structures were composed of ferrite and pearlite. Pearlite was formed since the cooling rates were less than 5°C/sec. in the temperature range of not higher than Ar_1 point + 50°C. In the cases of Symbols H-2, L-2 and 0-2, the average ferrite grain sizes were less than 20 μm. This meant that the average ferrite grain sizes reduced because the cooling rates were more than 10°C/sec. up to a temperature of Ar_1 point + 50°C after the end of hot rolling. In any cases of Symbols I-2, K-2, M-2 and N-2 where the structures were composed of ferrite and bainite, the content rates of bainite exceeded 15%; the upper limit of the preferable range. This was because the cooling after the end of hot rolling was commenced from a temperature higher than Ar_1 point + 50°C and, as a result, ferrite transformation did not proceed and thus the content rates of bainite increased. The yield ratios (YRs) of the 5%-prestrain specimens were in the range from 90 to 96%. YSs and TSs were higher in the cases of high bainite content rates than in the cases of-low bainite content rates.

Example 3

[0078] Example 3 relates to the third invention.

[0079] Steels having the components shown in Table 5 were produced into continuously cast slabs and then the slabs were hot rolled into steel sheets 10 mm in thickness. In the hot-rolling process: the slabs were heated to a temperature of 1,150°C; thereafter the hot rolling was finished at a temperature of 900°C (Ar_1 point + 170°C); the steel sheets were cooled at the cooling rate of 5°C/sec. up to a temperature of 780°C (Ar_1 point + 50°C) and thus ferrite transformation was caused; successively the steel sheets were cooled at the cooling rate of 30°C/sec. in the temperature range of not higher than 780°C (Ar_1 point + 50°C) and thus bainite and/or martensite were/was formed; and then the steel sheets were coiled in the temperature range from 400°C to 500°C.

[0080] The microstructures of the steel sheets are shown in Table 6. The tensile properties of a steel sheet were evaluated by using an as-rolled specimen of the steel sheet to which no working was applied and a specimen thereof to which 5%-prestrain was applied. 5%-Prestrain corresponds to the cold-working applied for forming a steel sheet 10 mm in thickness into a steel pipe 200 mm in diameter. In general, prestrain is applied so as to equal the value of t (steel pipe thickness)/D (steel pipe diameter) with respect to a steel pipe to be produced. The prestrain was given by the method wherein a tensile test specimen was pulled with a tensile tester and the pulling was stopped at the time when the strain reached 5%. The conditions of the tensile tests were the same as Example 1. The results of the evaluation are shown in Table 6.

[Table 5]

	Symbol	Chemical components (mass%)												
		C	Si	Mn	Al	Nb	N	Cu	Ni	Cr	Mo	V	Ti	B
Invention example	A-3	0.08	0.21	1.21	0.021	0.035	0.0032	0.001	0.002	0.004	0.003	0.004	0.003	0.00007
	B-3	0.12	0.33	0.95	0.026	0.051	0.0024	0.003	0.001	0.005	0.004	0.006	0.002	0.00005
	D-3	0.10	0.41	0.72	0.018	0.045	0.0051	0.002	0.005	0.004	0.002	0.003	0.015	0.00176
	E-3	0.15	0.52	0.83	0.028	0.053	0.0023	0.104	0.512	0.003	0.002	0.005	0.013	0.00005
	F-3	0.11	0.37	0.76	0.032	0.072	0.0041	0.005	0.004	0.587	0.573	0.225	0.015	0.00027
Comparative example	H-3	0.005	0.12	0.45	0.023	1.575	0.0030	0.003	0.001	0.002	0.004	0.003	0.002	0.00004
	I-3	0.42	0.15	0.48	0.048	0.003	0.0025	0.001	1.463	0.002	0.004	0.003	0.002	0.00003
	J-3	0.27	0.003	1.24	0.018	0.005	0.0158	0.002	0.003	0.007	0.003	0.875	0.002	0.00005
	K-3	0.10	1.48	1.85	0.024	0.001	0.0018	0.002	0.001	2.534	0.002	0.001	0.001	0.00005
	L-3	0.11	0.32	0.04	0.017	0.005	0.0035	0.001	0.004	0.003	2.438	0.002	0.002	0.00003
	M-3	0.13	0.27	2.58	0.042	0.003	0.0051	1.845	0.006	0.001	0.002	0.003	0.003	0.00006
	N-3	0.12	0.45	1.52	0.004	0.004	0.0046	0.002	0.005	0.003	0.004	0.004	0.005	0.01432
	O-3	0.04	0.31	0.93	0.115	0.006	0.0024	0.001	0.001	0.004	0.001	0.005	0.367	0.00008

[Table 6]

	Symbol	Metallographic structure				Tensile properties					
		Structure composition	Average ferrite grain size (μm)	Bainite content rate (volume%)	Martensite content rate (volume%)	As-rolled specimen			Specimen corresponding to t/D = 5%		
						YS (MPa)	TS (MPa)	YR (%)	YS (MPa)	TS (MPa)	YR (%)
Invention example	A-3	α + M	46	0	7	409	507	81	498	581	86
	B-3	α + B + M	35	7	9	491	635	77	611	716	85
	D-3	α + B + M	38	6	8	455	582	78	561	660	85
	E-3	α + B + M	82	10	13	593	782	76	751	870	86
	F-3	α + B + M	41	11	13	564	775	73	717	862	83
Comparative example	H-3	α	10	0	0	288	327	88	370	391	95
	I-3	α + B + M	19	40	44	723	838	86	905	957	95
	J-3	α + M	18	0	35	376	437	86	613	654	94
	K-3	α + B + M	33	22	23	347	408	85	517	552	94
	L-3	α + B + M	10	30	31	387	442	88	537	565	95
	M-3	α + B + M	32	22	33	367	431	85	569	616	93
	N-3	α + B + M	94	22	24	288	343	84	604	640	94
	O-3	α + P	8	0	0	345	393	88	495	520	95

α: Ferrite
B: Bainite
M: Martensite
P: Pearlite

t: Steel pipe thickness
D: Steel pipe outer diameter

[0081] In the cases of the invention examples Symbols A-3 to F-3, the steel components were within the ranges specified in the present invention, any of the structures was composed of ferrite and martensite, or ferrite, bainite and martensite, any of the average ferrite grain sizes was not smaller than 20 μm, and the bainite content rates and the martensite content rates were in the preferable range of not more than 15%. The yield ratios (YRs) of the 5%-prestrain specimens were in the range from 83 to 86%.

[0082] In the cases of the comparative examples Symbols H-3 to O-3, any of the steel components deviated from the ranges specified in the present invention. The structures were composed of ferrite in the case of Symbol H-3, and of ferrite and pearlite in the case of Symbol O-3. whereas, in the case of Symbol O-3, pearlite formed because the cooling rate was less than 5°C/sec. in the temperature range of not higher than Ar_1 point + 50°C, in the case of Symbol H-3, single ferrite phase formed because the C content was as low as 0.005% in addition to the influence of the low cooling rate similar to the case of Symbol O-3. in the cases other than Symbols K-3, M-3 and N-3, the average ferrite grain sizes were less than 20 μm. This meant that the average ferrite grain sizes reduced because the cooling rates were more than 10°C/sec. up to a temperature of Ar_1 point + 50°C after the end of hot rolling. In any cases of Symbols I-3, J-3, K-3, L-3, M-3 and N-3 where the structures contained martensite and bainite, the bainite content rates and martensite content rates exceeded 15%; the upper limit of the preferable range. This was because the cooling after the end of hot rolling was commenced from a temperature higher than Ar_1 point + 50°C and, as a result, ferrite transformation did not proceed and thus the bainite content rates or the martensite content rates increased. The yield ratios (YRs) of the 5%-prestrain specimens were in the range from 93 to 95%.

[0083] The present invention makes it possible to: reduce the production cost of a low yield ratio steel pipe by suppressing the Cr content; enhance tensile strength at the ordinary temperature by suppressing the formation of Cr oxides that deteriorate the quality of a weld and raising the upper limit of the C content; and thus obtain a low yield ratio steel pipe.

Claims

1. A steel pipe having a low yield ratio, **characterized in that**: the steel pipe contains, in mass, 0.01 to 0.20% C, 0.05 to 1.0% Si, 0.1 to 2.0% and 0.001 to 0.05% A1, with the balance consisting of Fe and unavoidable impurities; the microstructure of the steel pipe is composed of ferrite and additionally one or both of pearlite and cementite; and the average size of the ferrite grains is not smaller than 20 μm.

2. A steel pipe having a low yield ratio according to claim 1, **characterized in that** the microstructure of the steel pipe contains spheroidized pearlite or spheroidized cementite.

3. A steel pipe having a low yield ratio according to claim 2, **characterized in that** the average size of pearlite grains or cementite grains is not larger than 20 μm.

4. A steel pipe having a low yield ratio according to any one of claims 1 to 3, **characterized in that** the steel pipe contains, in mass, one or both of 0.01 to 0.5% Nb and 0.001 to 0.01% N.

5. A steel pipe having a low yield ratio **characterized in that**: the steel pipe contains, in mass, 0.03 to 0.20% C, 0.05 to 1.0% Si, 0.1 to 2.0% Mn, 0.001 to 0.05% A1, 0.01 to 0.5% Nb and 0.001 to 0.01% N, with the balance consisting of Fe and unavoidable impurities; the microstructure of the steel pipe is compose of ferrite and bainite; and the average size of the ferrite grains is not smaller than 20 μm.

6. A steel pipe having a low yield ratio according to claim 5, **characterized in that** the content rate of bainite is, in volume fraction, in the range from 1 to 15%.

7. A steel pipe having a low yield ratios **characterized in that**: the steel pipe contains, in mass, 0.03 to 0.20% C, 0.05 to 1.0% Si, 0.1 to 2.0% Mn, 0.001 to 0.05% Al, 0.01 to 0.5% Nb and 0.001 to 0.01% N, with the balance consisting of Fe and unavoidable impurities; the microstructure of the steel pipe is composed of ferrite, martensite and bainite, or ferrite and martensite; and the average size of the ferrite grains is not smaller than 20 μm.

8. A steel pipe having a low yield ratio according to claim 7, **characterized in that** the content rate of bainite is, in volume fraction, in the range from 1 to 15% and/or that of martensite is, in volume fraction, in the range from 1 to 15%.

9. A steel pipe having a low yield ratio according to any one of claims 1 to 8, **characterized in that** the steel pipe

contains, in mass, one or both of 0.005 to 0.1% Ti and 0.0001 to 0.005% B.

10. A steel pipe having a low yield ratio according to any one of claims 1 to 9, **characterized in that** the steel pipe contains, in mass, one or more of 0.01 to 0.5% v, 0.01 to 1% Cu, 0.01 to 1% Ni, 0.01 to 1% Cr and 0.01 to 1% Mo.

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(54) Steel pipe having low yield ratio

(57) The present invention provides a steel pipe having a low yield ratio and is: a steel pipe having a low yield ratio, wherein the steel pipe contains, in mass, 0.01 to 0.20% C, 0.05 to 1.0% Si, 0.1 to 2.0% Mn and 0.001 to 0.05% Al, the microstructure of the steel pipe is composed of ferrite and pearlite, or ferrite and cementite, and the average size of the ferrite grains is not smaller than 20 μm; and a steel pipe having a low yield ratio, wherein the steel pipe contains, in mass, 0.03 to 0.20% C, 0.05 to 1.0% Si, 0.1 to 2.0% Mn, 0.001 to 0.05% Al, 0.01 to 0.5% Nb and 0.001 to 0.01% N, the microstructure of the steel pipe is composed of ferrite and bainite, or ferrite, martensite and bainite, or ferrite and martensite, and the average size of the ferrite grains is not smaller than 20 μm.

EP 1 382 703 A3

European Patent Office

EUROPEAN SEARCH REPORT

Application Number
EP 03 01 5517

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The present search report has been drawn up for all claims

Place of search	Date of completion of the search	Examiner
Munich	30 January 2004	Swiatek, R

CATEGORY OF CITED DOCUMENTS

X : particularly relevant if taken alone
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A : technological background
O : non-written disclosure
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E : earlier patent document, but published on, or after the filing date
D : document cited in the application
L : document cited for other reasons

& : member of the same patent family, corresponding document

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EUROPEAN SEARCH REPORT

Application Number
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Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
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The present search report has been drawn up for all claims

Place of search	Date of completion of the search	Examiner
Munich	30 January 2004	Swiatek, R

CATEGORY OF CITED DOCUMENTS

X : particularly relevant if taken alone
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CLAIMS INCURRING FEES

The present European patent application comprised at the time of filing more than ten claims.

- [ ] Only part of the claims have been paid within the prescribed time limit. The present European search report has been drawn up for the first ten claims and for those claims for which claims fees have been paid, namely claim(s):

- [ ] No claims fees have been paid within the prescribed time limit. The present European search report has been drawn up for the first ten claims.

LACK OF UNITY OF INVENTION

The Search Division considers that the present European patent application does not comply with the requirements of unity of invention and relates to several inventions or groups of inventions, namely:

see sheet B

- [X] All further search fees have been paid within the fixed time limit. The present European search report has been drawn up for all claims.

- [ ] As all searchable claims could be searched without effort justifying an additional fee, the Search Division did not invite payment of any additional fee.

- [ ] Only part of the further search fees have been paid within the fixed time limit. The present European search report has been drawn up for those parts of the European patent application which relate to the inventions in respect of which search fees have been paid, namely claims:

- [ ] None of the further search fees have been paid within the fixed time limit. The present European search report has been drawn up for those parts of the European patent application which relate to the invention first mentioned in the claims, namely claims:

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LACK OF UNITY OF INVENTION SHEET B

Application Number
EP 03 01 5517

The Search Division considers that the present European patent application does not comply with the requirements of unity of invention and relates to several inventions or groups of inventions, namely:

1. claims: 1-4,9,10

   Steel pipe made of manganese steel having a microstructure composed of ferrite and pearlite or cementite wherein an average grain size of ferrite grains is not smaller than 20 micrometer

   ---

2. claims: 5,6,9,10

   Steel pipe made of manganese steel containing niobium and nitrogen having a microstructure composed of ferrite and bainite wherein an average grain size of ferrite grains is not smaller than 20 micrometer

   ---

3. claims: 7-10

   Steel pipe made of manganese steel containing niobium and nitrogen having a microstructure composed of ferrite and marensite or martensite and bainite wherein an average grain size of ferrite grains is not smaller than 20 micrometer

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ANNEX TO THE EUROPEAN SEARCH REPORT ON EUROPEAN PATENT APPLICATION NO. EP 03 01 5517

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